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ELECTROMAGNETIC AND ELECTROMECHANICAL MACHINES

Third Edition

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Dedicated to:

*The memory of Leander W. Matsch
The family of J. Morgan J. Derald
becca, John, Jr., and his mother
Our students, past, present, and future*

Electromagnetic and Electromechanical Machines, Third Edition

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4/SYNCHRONOUS MACHINES

4-2 WAVEFORM

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(General Electric Company.)

For example, a certain 432,000-r/min generator has a rated armature current of 1940 A.

For a sinusoidal voltage under production of good waveform among several slots per phase is that span less than 180° in angle among several slots per pole of salient-pole rotors so that the field winding is in length toward the

cylindrical rotors along with a number of poles. One pole and its

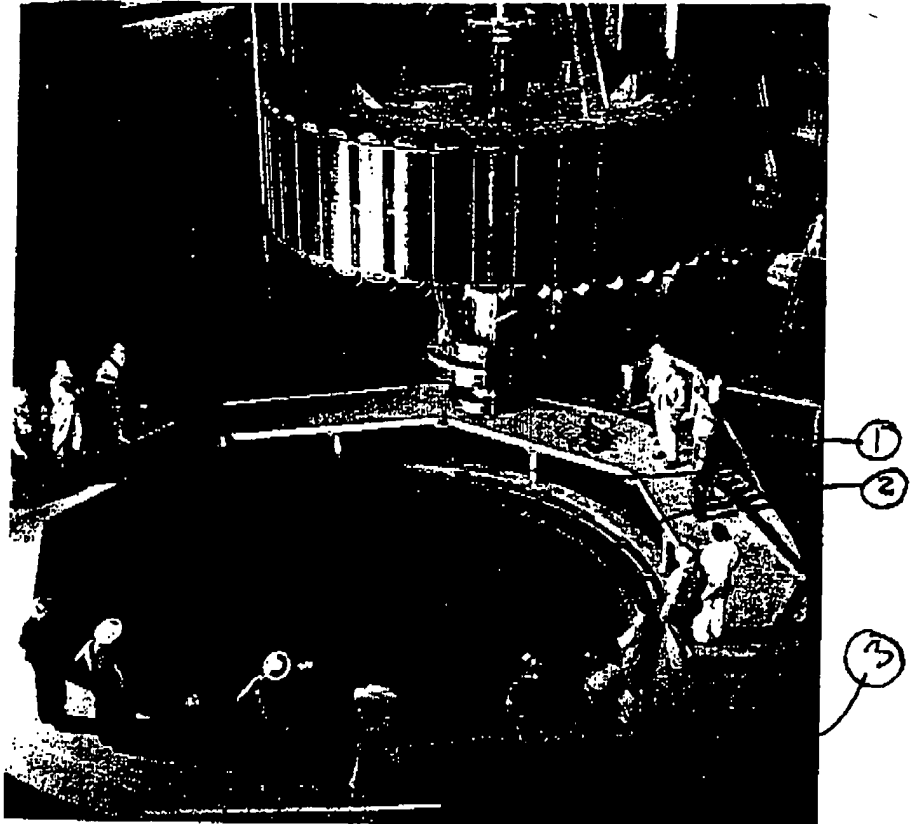


Figure 4-3 Salient-pole rotor being lowered into the stator of a hydrogenerator. (Courtesy General Electric Company.)

The associated field coil of a salient-pole rotor is shown in Fig. 4-5(d). The stator slots in which the armature winding is embedded are not shown for reasons of simplicity. The approximate path taken by the field flux, not including leakage flux, is indicated by the dashed lines in Fig. 4-5(a), (b), and (d). The field coils in Fig. 4-5(c) are represented by filaments but actually (except for the insulation between turns and between the coil sides and the slot) practically fill the slot more nearly in keeping with Fig. 4-6.

The stepped curve in Fig. 4-6 represents the waveform of the mmf produced by the distributed field winding if the slots are assumed to be completely filled by the copper in the coil sides instead of containing current filaments. The shape of the mmf wave may be verified for this assumption by taking line integrals of H around appropriate paths. The sinusoid indicated by the dashed line in Fig. 4-6 represents approximately the fundamental component of the mmf wave.

The air gap in cylindrical-rotor machines is practically of uniform length

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